

SHAKE THE FUTURE.



Étude en soufflerie atmosphérique du sillage d'une éolienne flottante

Sandrine Aubrun,
Professor in Centrale Nantes
Research lab on Hydrodynamics, Energetics and Atmospheric Environment (LHEEA)

GDR EOL-EMR Day, November 25, 2021



FLOATEOLE project

Experimental characterization of the wave impact on the unsteady aerodynamical behavior of floating wind turbines

- 2017-2022
- Grant 164k€
- Funders / Supports



© Centrale Nantes





FLOATEOLE project

L'équipe-projet



Sandrine AUBRUN
Prof. ECN, éq. SEMREV+



Boris CONAN
MCF ECN, éq. DAUC



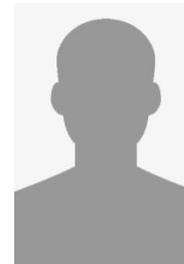
Yves PERIGNON
IR CNRS, éq. SEM-REV+



Jean-Marc ROUSSET
IR ECN, éq. SEM-REV+



Benjamin SCHLIFFKE
Doct. Éq. DAUC/SEMREV+



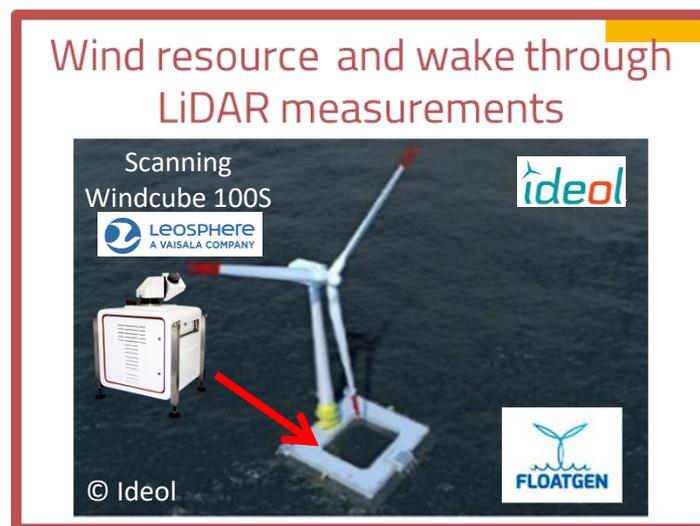
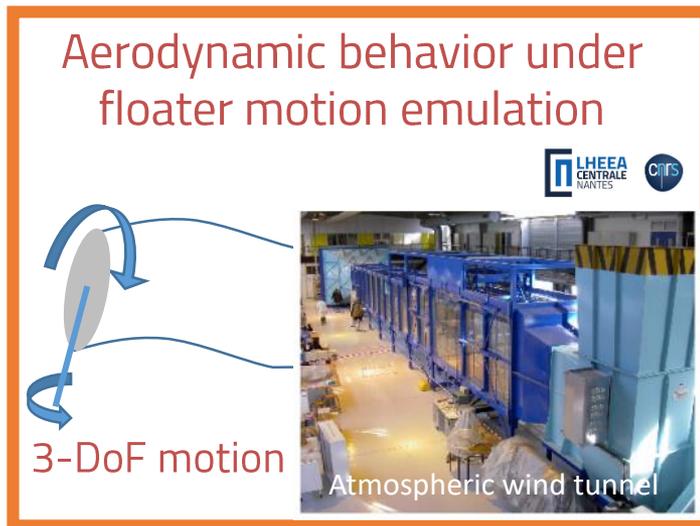
Antonin HUBERT
Doct. Éq. DAUC/SEMREV+



Post-doc
2022

Methodology

- Multidisciplinary approach to study the wind – wave – structure coupling
- Experiments performed in controlled and real conditions (wind tunnel and sea test site, respectively)



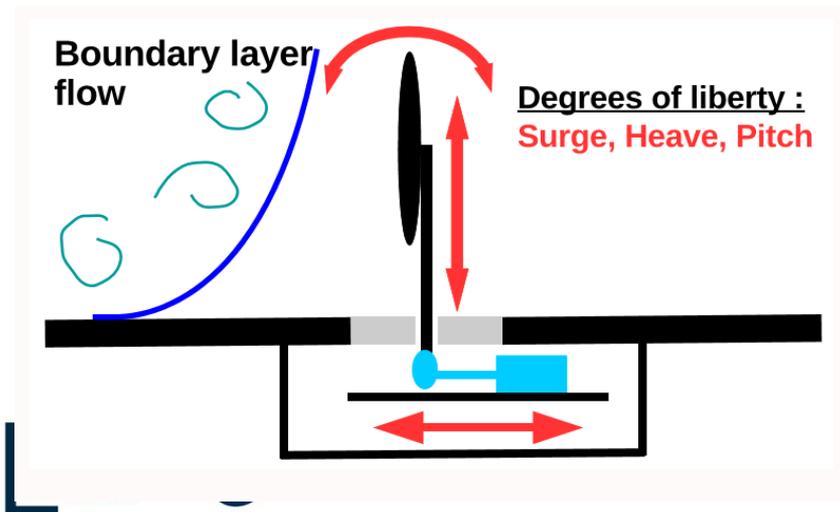
Scientific and technical challenges :

- Does the floater motion have an impact on the wind turbine wake development?
- Can the signature of the motion be found in the wake?
- Wind tunnel testing: Floater motion emulation at very reduced scale
- Sea testing: scanning LiDAR measurement on floating structures

Technical challenges

- **Wind tunnel experiments**

- Design a motion system that can emulate the floaters movements in different sea states
 - From idealised to extreme cases
 - For a reduction scale of 1:400
- => High accelerations



- **Onsite experiments**

- Mitigate the influence of floater motions on the LiDAR measurements
 - Stabilizing platform
 - Control of the scanning head



Scanning Windcube



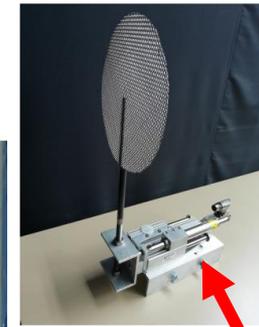
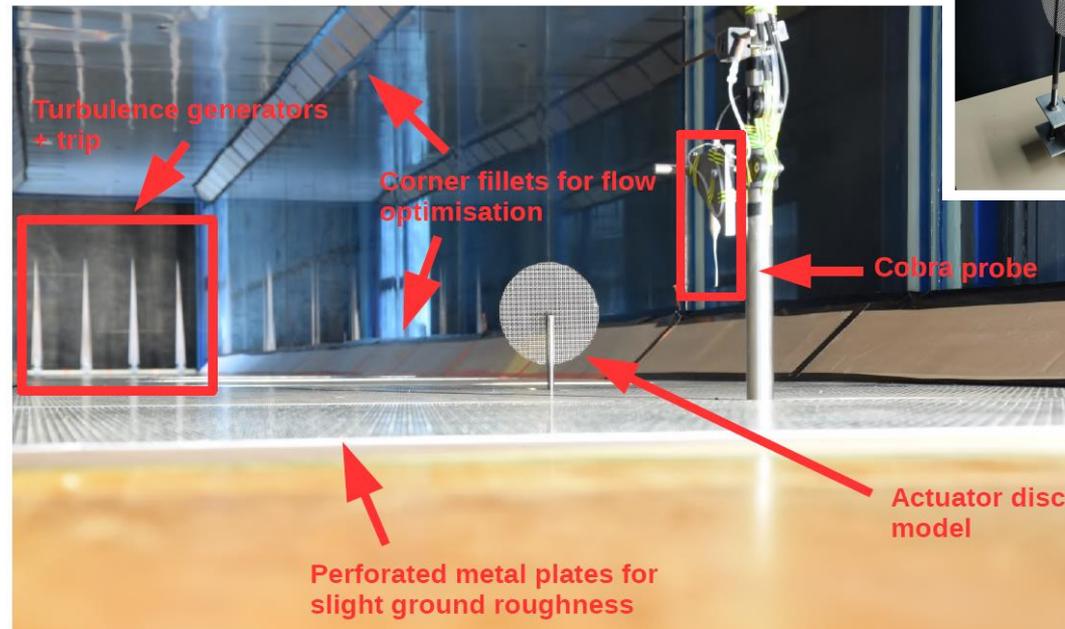
Credit: ©Ideol



Experimental set-up

Wind tunnel testing: Floater motion emulation at very reduced scale

Set-up in the atmospheric wind tunnel (Centrale Nantes/LHEEA)



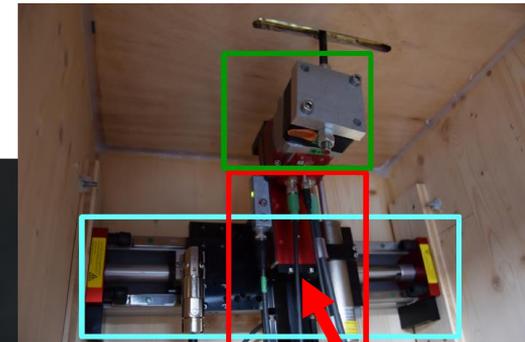
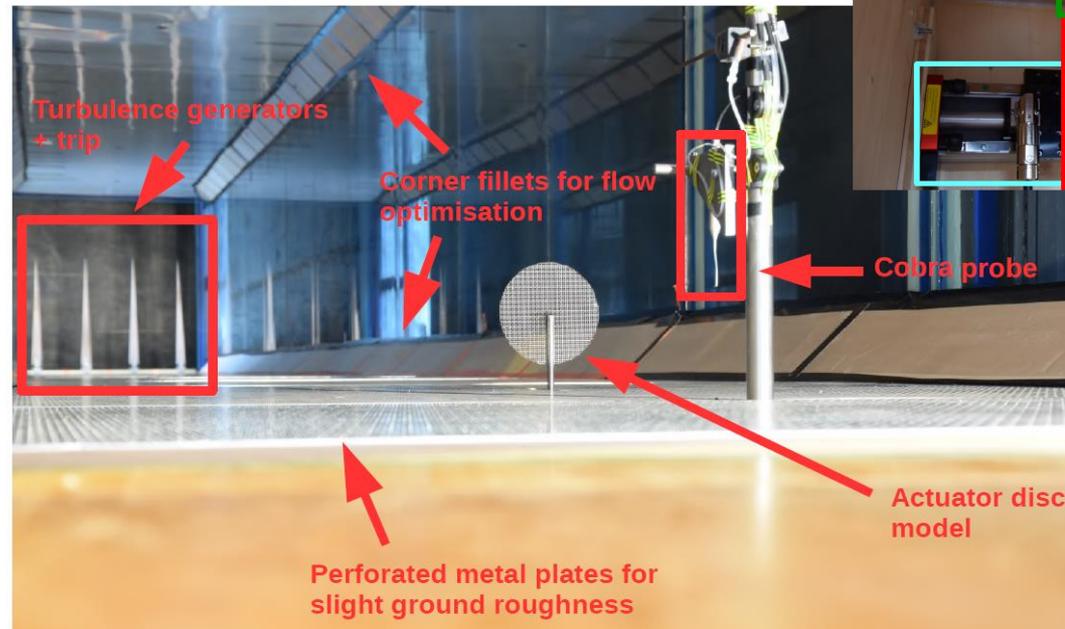
1DOF motion (Surge)

Reduction scale 1:500
(No possible Reynolds similarity)
+
Far-wake
=
Actuator disc model (porous disc)

Experimental set-up

Wind tunnel testing: Floater motion emulation at very reduced scale

Set-up in the atmospheric wind tunnel (Centrale Nantes/LHEEA)



Reduction scale 1:500

(No possible Reynolds similarity)

+

Far-wake

=

Actuator disc model (porous disc)

Experimental set-up

Scaling driven by wind tunnel capacities

| Scaling factor | Value |
|----------------|---------------------|
| Geometric | $\Lambda_L = 500$ |
| Kinematic | $\Lambda_v = 2.5$ |
| Time | $\Lambda_t = 200$ |
| Frequency | $\Lambda_f = 0.005$ |

Scaling driven by disc aerodynamics

$$f_{red} = \frac{f \cdot D}{U_{ref}} = St_D$$

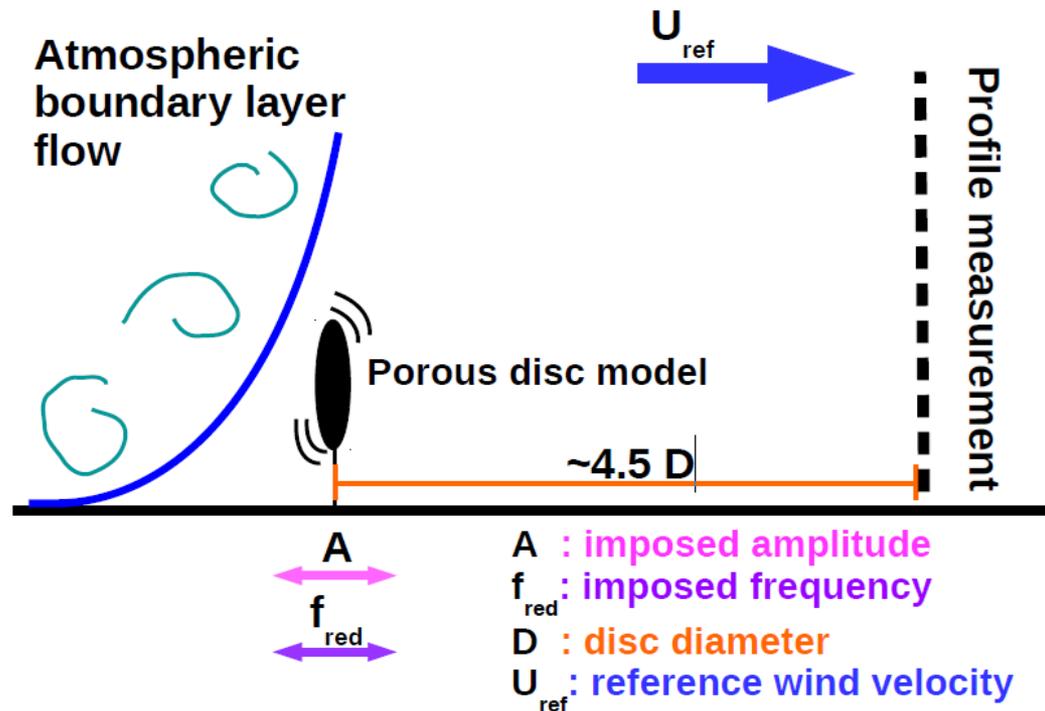
Surge specifications

\Rightarrow Characteristic $A = L = 0.125D$

\Rightarrow Characteristic $f_{red} = \frac{f \cdot D}{U_{ref}} = 0.1$

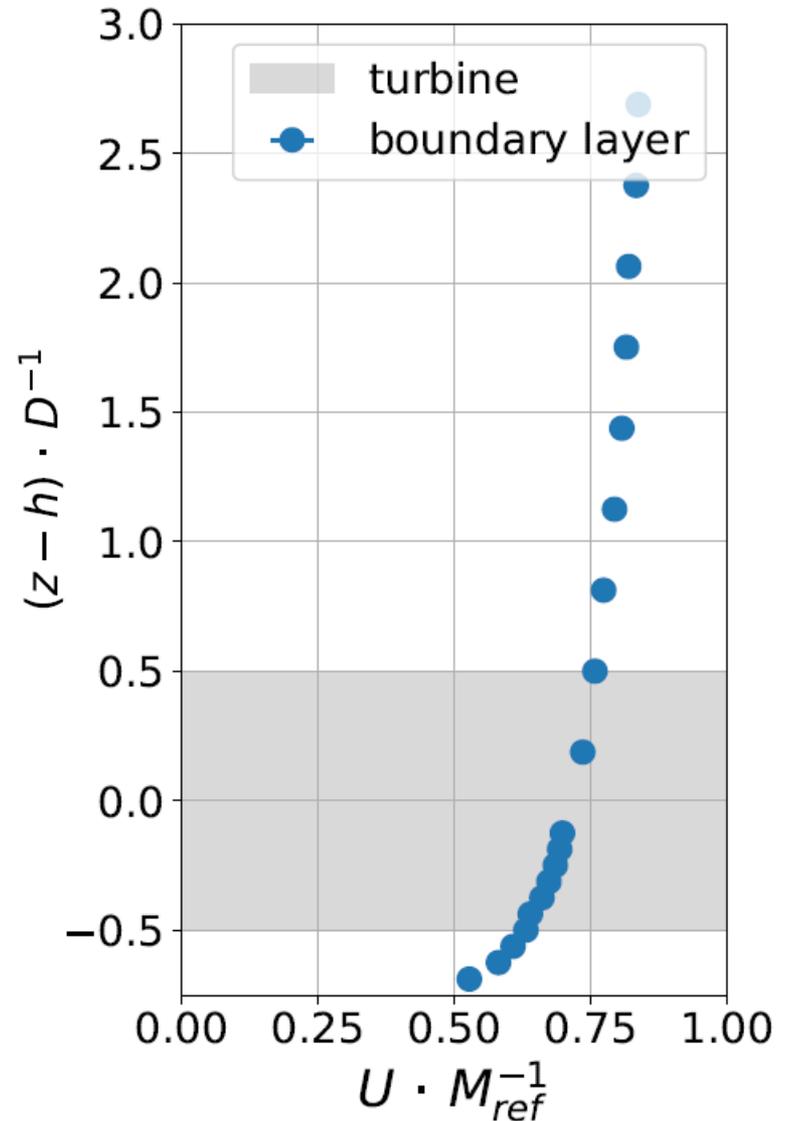
Floating Wind turbine scaling

| | Full scale | Wind tunnel | Name |
|----------------------------|------------|-------------|-------|
| Rotor diameter | 80 m | 16 cm | D |
| Nacelle height | 60 m | 12 cm | h |
| Char. floater surge motion | 10 m | 2 cm | L |
| Char. floater surge freq. | 0.01 Hz | 2 Hz | f_s |

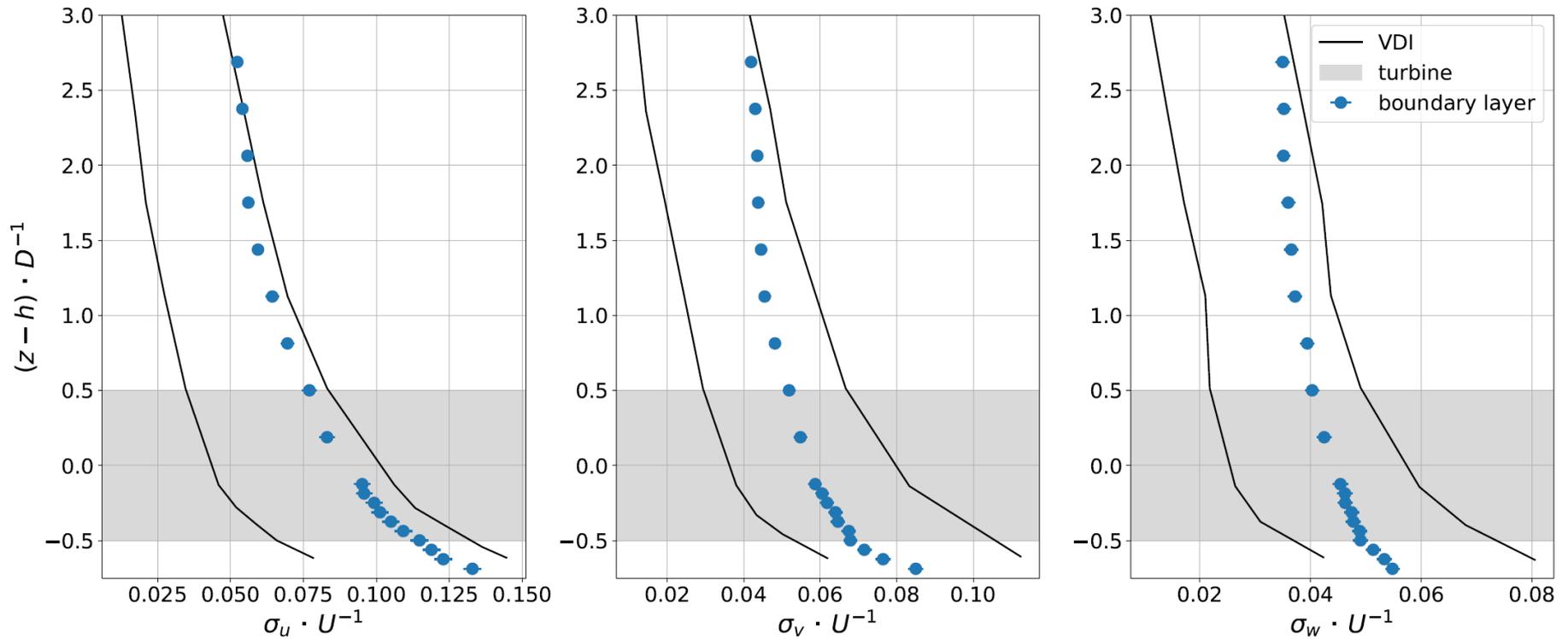


Modelled atmospheric boundary layer

| Roughness class | Target values | Modelled |
|-----------------|---------------------------------|----------------------|
| Type of terrain | ice, snow, water surface | water surface |
| z_0 [m] | 10^{-5} to 5×10^{-3} | 5.5×10^{-6} |
| α | 0.08 to 0.12 | 0.11 |
| d_0 [m] | ≈ 0 | 0 |



Modelled atmospheric boundary layer



Atmospheric boundary layer specifications

VDI 3783 versus IEC guidelines

Table: Comparison of VDI Guideline 3783 (VDI, 2000) for a modelled offshore boundary layer and IEC 61400-3 design load cases for offshore wind turbines (IEC, 2009). The reference height is the nacelle in this table. For neutral stratification.

| Quantity | VDI Guideline 3783 | IEC 61400-3 | Modelled |
|----------------------|--------------------|---|----------------|
| I_{ref} | - | 12% | - |
| I_u | 5% – 10% | $I_{ref} \cdot (0.75 \cdot V_{hub} + b) b = 5.6m/s$ | $\approx 9\%$ |
| α | 0.08 – 0.12 | 0.14 | 0.11 |
| validity of α | entire profile | rotor swept area | entire profile |
| stratification | neutral | no mention | neutral |

- IEC 61400-3 overestimates turbulence intensity (especially at lower velocities; see the following slide) and α compared to the VDI.
- Calculating α according to IEC with our data results in $\alpha = 0.12$
- Calculating I_u according to IEC with our (rescaled) data results in $I_u \approx 22\%$

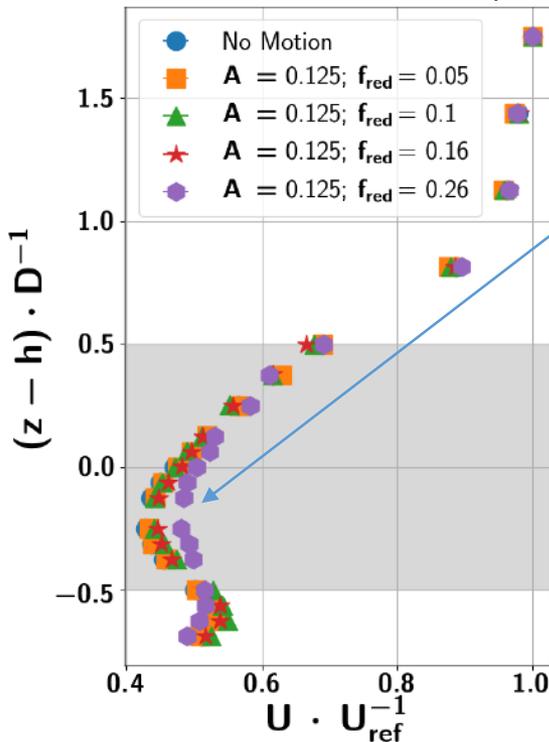
Mean velocity profiles

Impact of platform motions on far-wake properties

Imposed frequency-varying

Surge motion (fore-aft translation)

Vertical profiles of the Mean normalised velocity

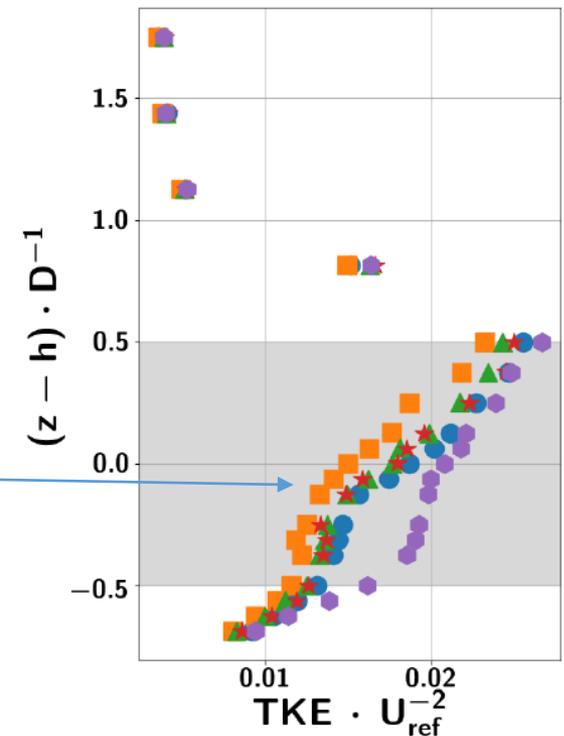


Vertical profiles of the mean velocity not significantly changed by the imposed motion

- the turbulent kinetic energy is disturbed in the rotor-swept-area
- Most of the frequencies of motion correspond to a loss of TKE when compared to the no motion reference case

4.6D downstream

Vertical profiles of the normalised turbulent kinetic energy (TKE)



Velocity fluctuation spectra

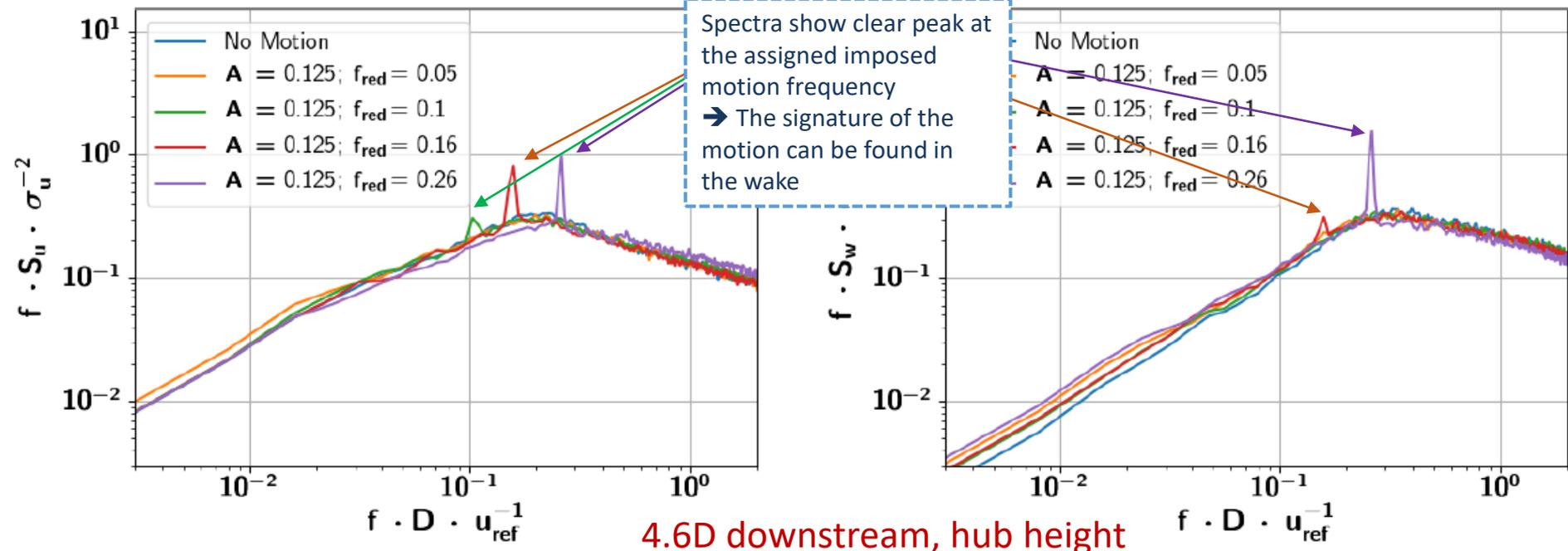
Impact of platform motions on far-wake properties

Imposed frequency-varying

Surge motion (fore-aft translation)

Spectra of the longitudinal velocity component u

Spectra of the vertical velocity component w



Velocity fluctuation spectra

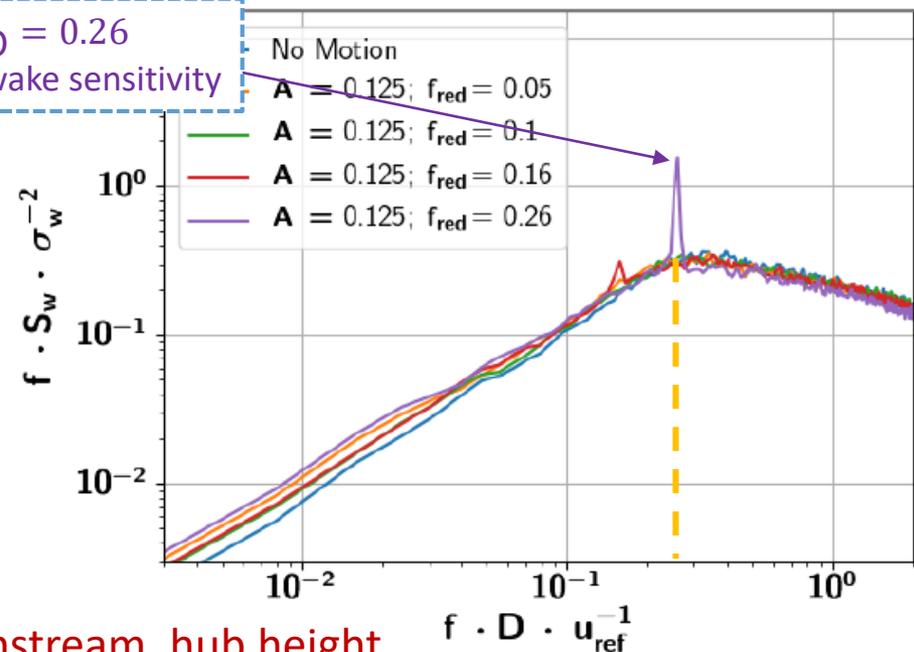
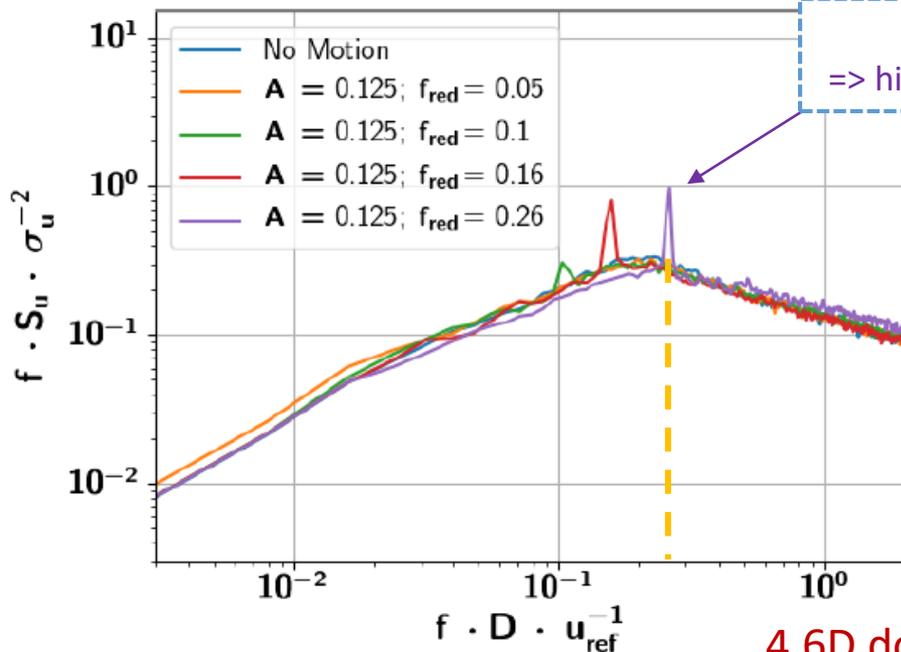
Impact of platform motions on far-wake properties

Imposed frequency-varying

Surge motion (fore-aft translation)

Spectra of the longitudinal velocity component u

Spectra of the vertical velocity component w



4.6D downstream, hub height

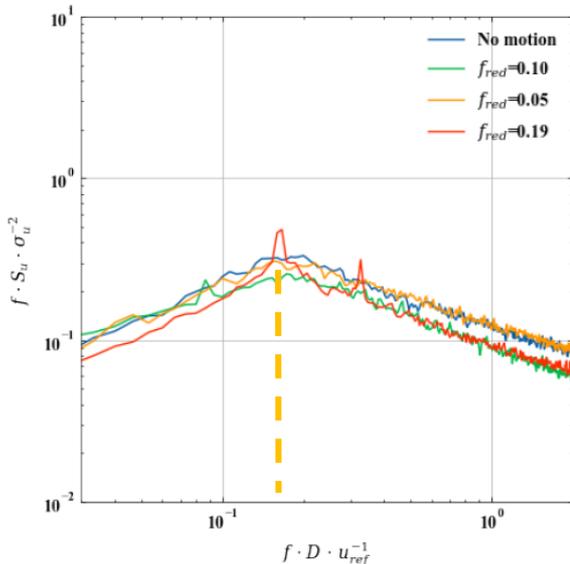
Velocity fluctuation spectra

Impact of platform motions on far-wake properties

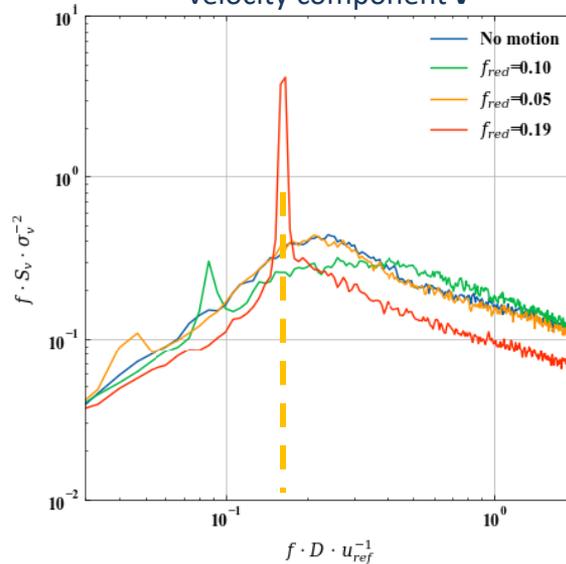
Imposed frequency-varying

Sway motion (side-to-side translation)

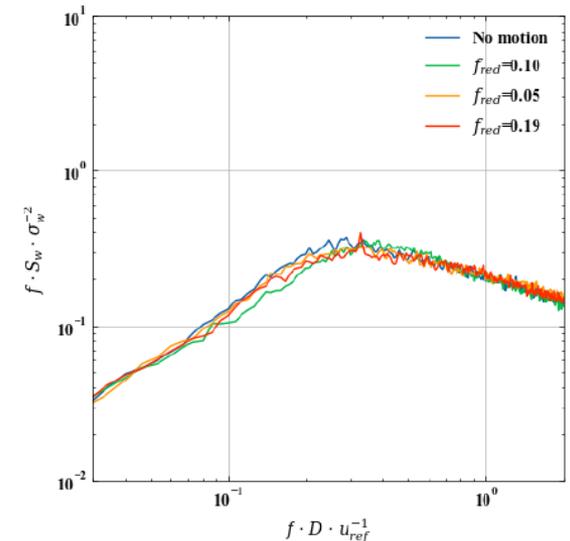
Spectra of the longitudinal velocity component u



Spectra of the vertical velocity component v



Spectra of the vertical velocity component w



4.6D downstream, hub height

Idealised Motions

- Can the signature of the harmonic motion be found in the far-wake? **Yes!** (if the motion is sufficiently strong and depends on the motion frequency)
- Is this indicative of faster wake recovery? **Yes, but only a little...**

Next steps

- Regular and irregular 3DOF motions (surge, sway, pitch or roll)
- Wake meandering characterisation
- Wake interactions of two floating wind turbines



Final comments on the project strategy

Wind turbine far-wake characterisation

Wind tunnel experiments

- Controlled environmental conditions
- Separate the contribution of motions & physical mechanisms to the wake modifications
- Challenges to work a reduced scale
- Upscaling?

Full scale measurement

- Uncontrolled and constantly changing environmental conditions
- Huge technical challenges in offshore conditions (equipment integrity and measurement reliability)
- **But real life!**